

# **CIGRE GOTF 2019 - Phase Angles as a Proxy for Voltage Stability**

Michael R. Richardson  
AMERICAN ELECTRIC POWER













# Agenda

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- AEP Overview
- Highpoints of AEP 2016 CIGRE GOTF paper on TVSI voltage stability.
- Phase Angles as a Proxy for Voltage Stability
- Conclusions
- Appendix – Voltage Stability Triangle Program

# AEP Overview

## 2018 COMPANY OVERVIEW

	Number of Employees	<b>17,582</b>		Transmission	<b>40,000 miles</b>
	Regulated & Competitive Customers	<b>5.8 million</b>		Distribution	<b>220,000 miles</b>
	Service Territory	<b>200,000 square miles</b>		Total Generating Capacity (owned & PPA)	<b>32,000 MW</b>
	Total Revenues	<b>\$16.2 billion</b>		Total Renewable Portfolio*	<b>5,272 MW</b>
	Capital Investments	<b>\$6 billion</b>		Total Assets	<b>\$68.8 billion</b>
	Cash Dividends Per Share	<b>\$2.53</b>		Charitable Giving	<b>\$25.5 million</b>

\* Includes expected capacity as of year-end 2019.

# Highpoints of AEP 2016 CIGRE GOTF paper on TVSI Voltage Stability

# Highpoints of AEP 2016 CIGRE GOTF paper

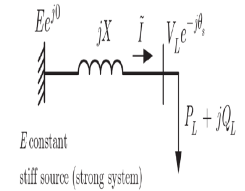
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- IEEE/CIGRE Joint Task Force Classification of Power System Stability
  - Long Term Voltage Stability using static analysis
- Triangle Voltage Stability Index – TVSI
  - Uses ratio of  $V_l$  and  $V_u$
  - $TVSI = V_l / V_u$
- Next two slides demonstate  $V_l$ ,  $V_u$ , and TVSI

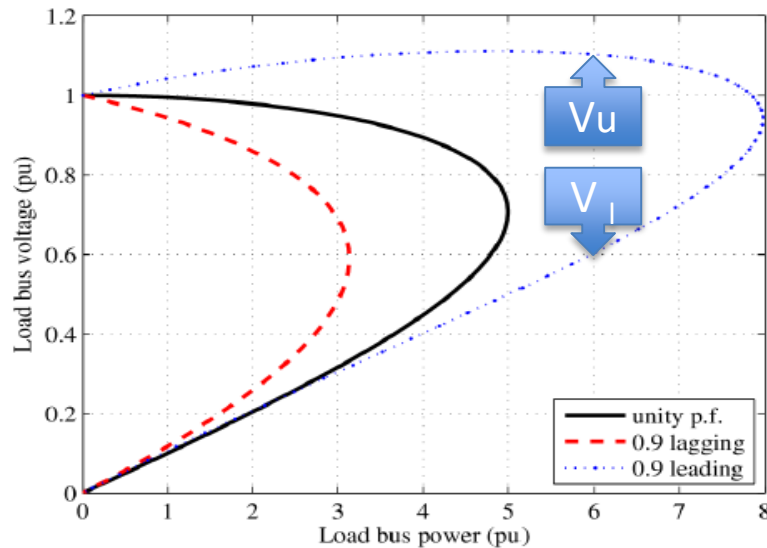
# Highpoints of AEP 2016 CIGRE GOTF paper

Single-Load, Stiff Bus System

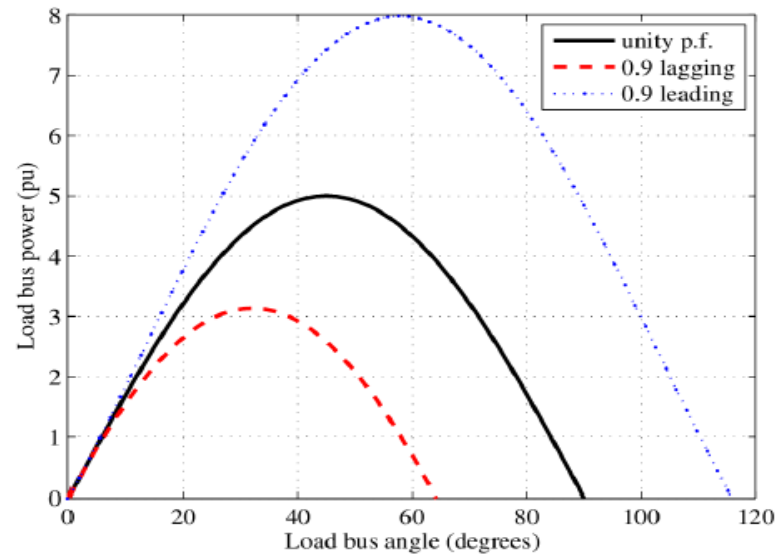
## PV Curves and Angle Separation



- Single-load VSA with constant power factor:
- Load bus angle (angle separation) is seldom analyzed in VSA

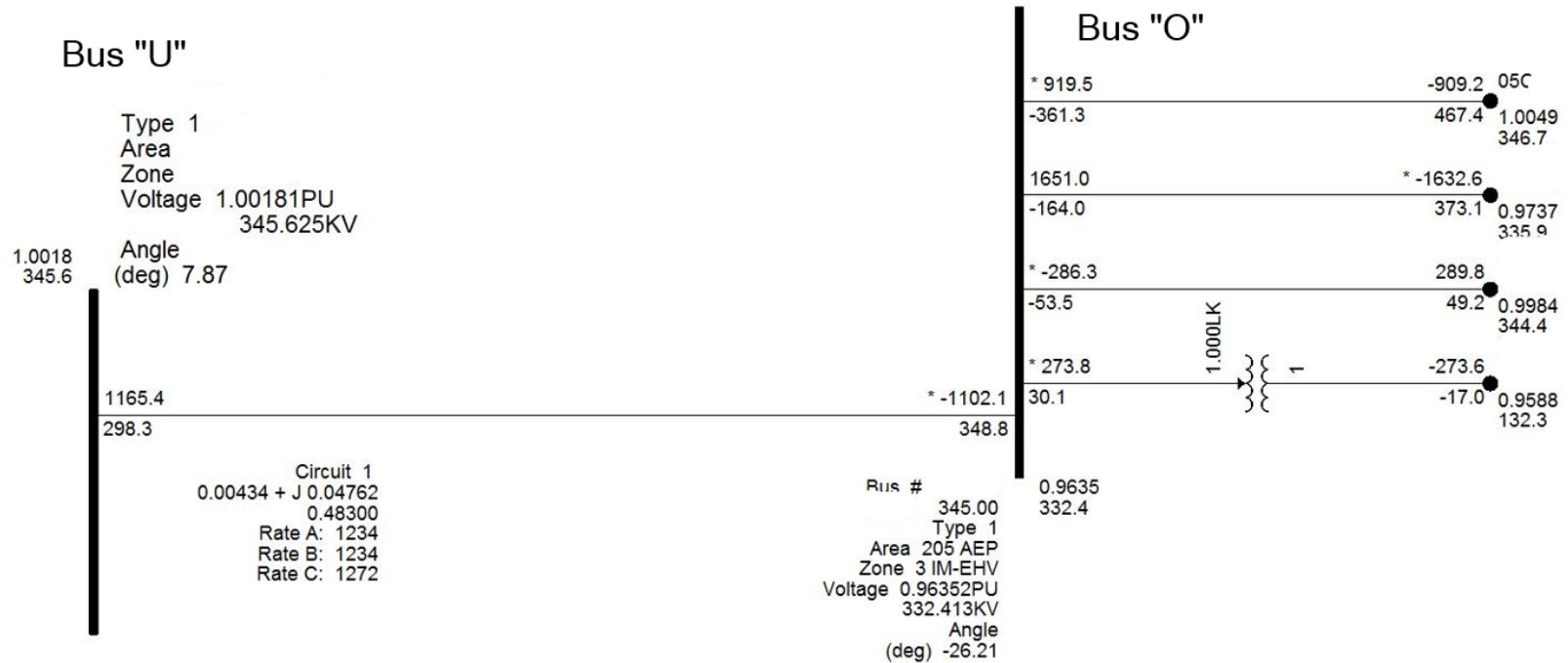


PV Curves



Power vs. Angle Separation

# TVSI, Voltage Drop, & Phase Angle Across a Branch



What's the voltage drop across the O -U 345kV path?

1.  $345.6 - 332.4 = 13.2\text{kV}$ ?
2.  $345.6@7.87 - 332.4@-26.21$ ?

Ans: **It's #2; 199kV**

**TVSI =  $V_1 / V_u = 199/332.4 = 0.5987$ ; Delta Phase Angle = 34.08 degrees**

# Phase Angles as a Proxy for Voltage Stability



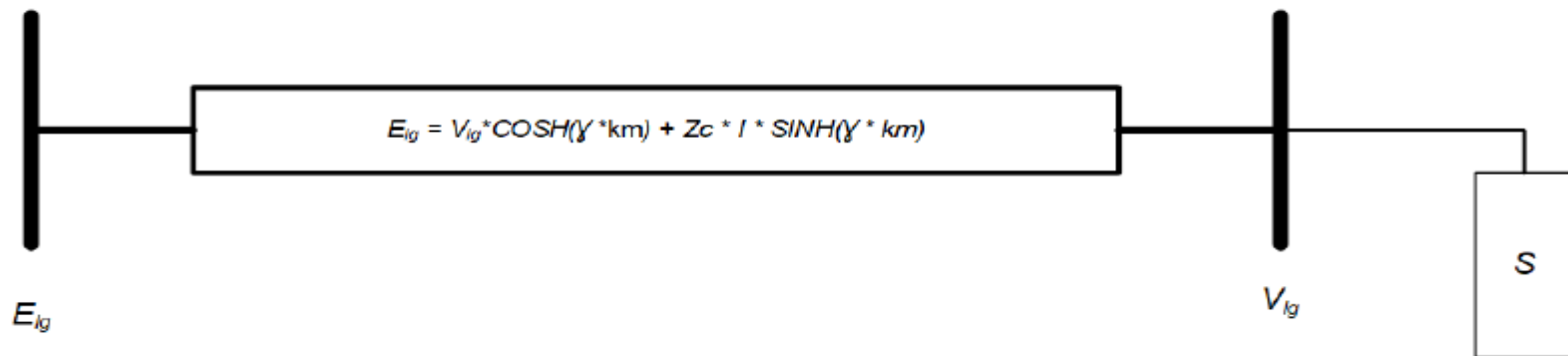


# Phase Angles & NERC

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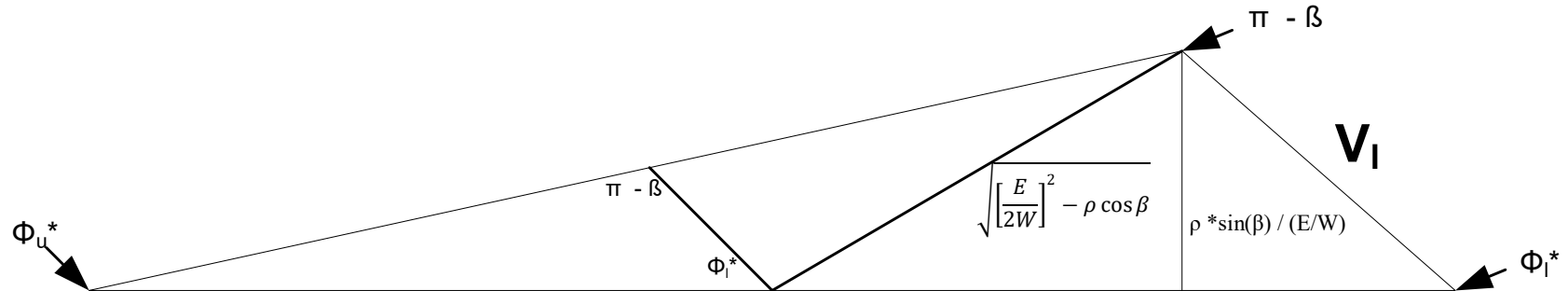
- NERC Standards
  - TOP 002-4 R1 has a phase angle requirement for the Operational Planning Analysis.
  - TOP 001-4 R13 has a phase angle requirement for the Real-time Assessment.
- NERC Phase Angle Monitoring technical reference document dated June 2016 notes that voltage stability and phase angles are related.

# Distributed Parameter Transmission Line



- Distributed Parameter Transmission line with
  - $E$  – Source voltage
  - $V$  – Load voltage
  - $S$  – Load  $S$
  - $Y$  – Propagation constant
  - $Z_c$  – Characteristic impedance
- The next slide displays a Voltage Stability Triangle that encapsulates the distributed parameters of transmission line.
  - Use triangle to describe the voltage stability index TVSI and determine the **phase angle**  $\phi_u$  of the load voltage  $V$ .

# Voltage Stability Triangle

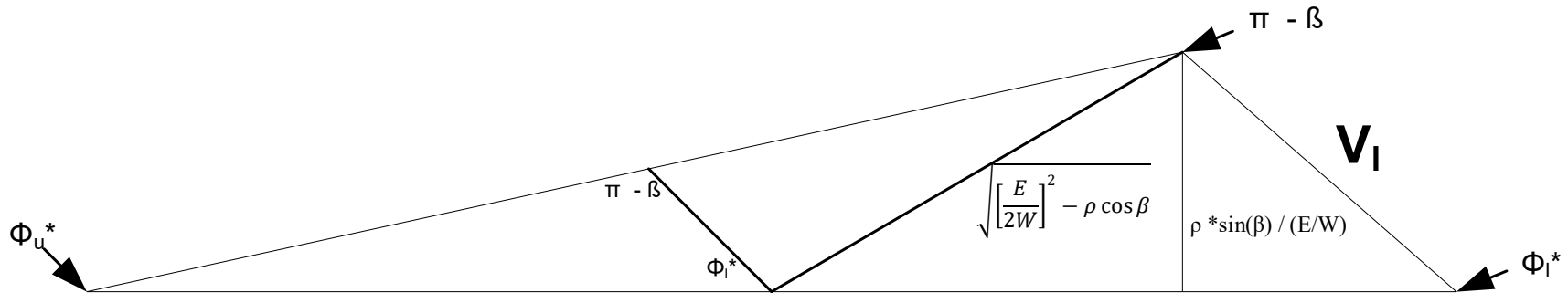


- $V_u$  is the load voltage magnitude on the upper side of the PV curve.
  - $V_l$  is the voltage magnitude on the lower side of the PV curve.
- The voltage stability index **TVSI** equals  $V_l/V_u$ .
  - TVSI approaches 1 when we are near the apex of the PV curve.
- The **phase angle**  $\phi_u$  is the angle of the load voltage  $V_u$  with respect to the source voltage  $E$ .
- $W$  is a factor that elongates the source voltage.
  - For a 250km line,  $W$  elongates the voltage by about 5%.

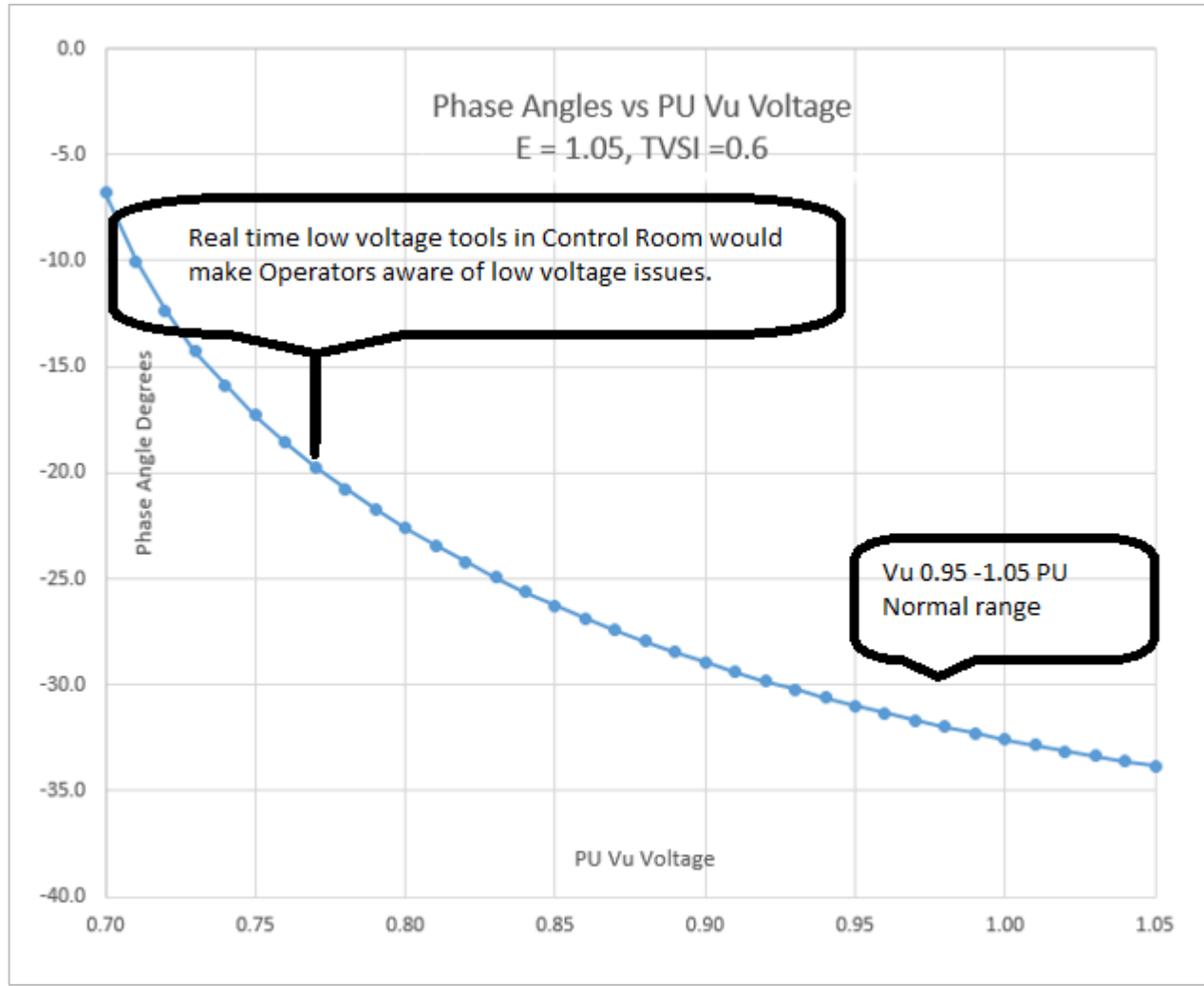


# Voltage Stability Triangle

- Use the triangle as a thinking tool.
- What is the **phase angle**  $\phi_u$  for various  $V_u$  voltages and a given TVSI ( $V_l / V_u$ ).
  - What load  $S$  drives the condition.

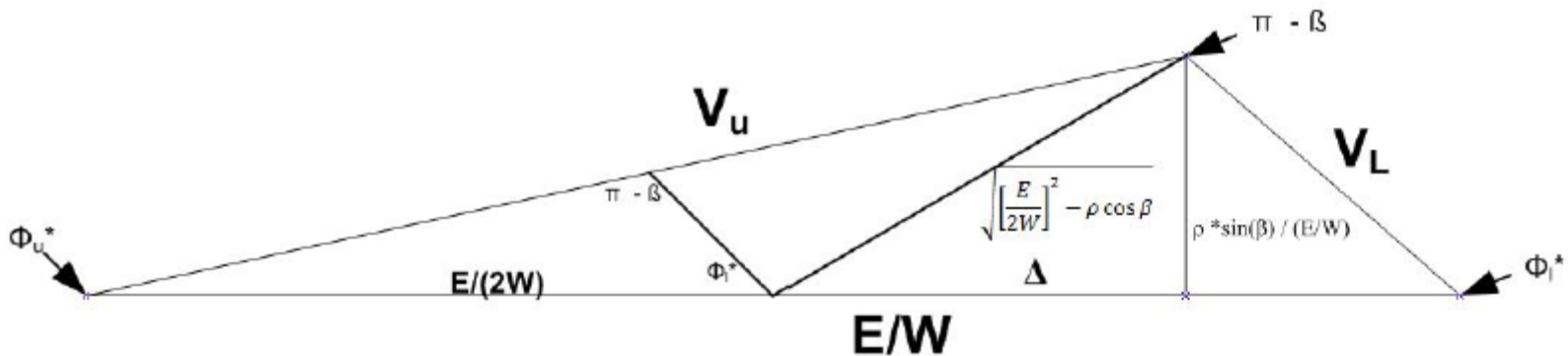


# Constant TVSI and Phase Angles



# Voltage Stability Triangle

- Next three slides examine **phase angle  $\phi_u$**  associated with low voltages and normal voltages.
  - Show the associated load  $S$ .



# Low Voltages, Lagging PF Load with TVSI=0.6

- 1.) Given:

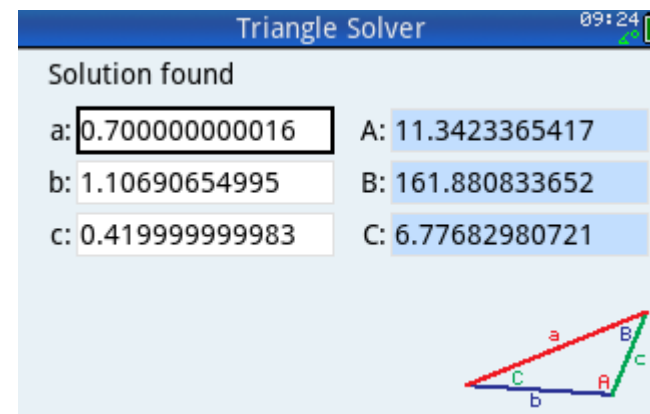
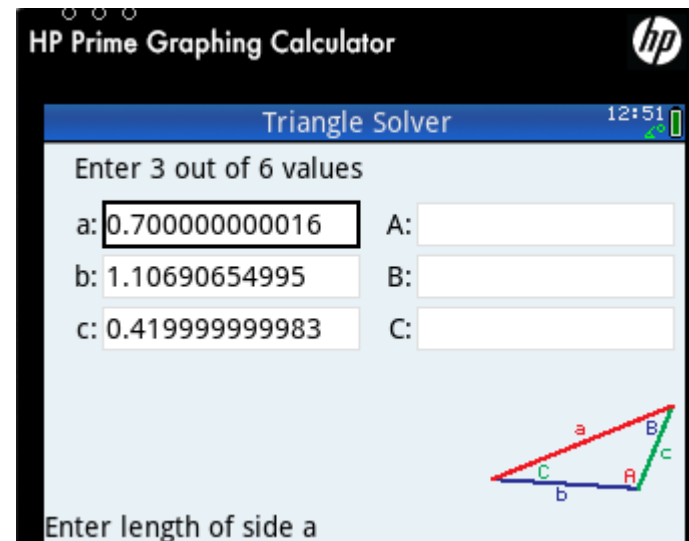
E: 1.05	KV: 345
P: 1.330807331	Q: 3.4201208886
$\alpha$ : 0.066/1,000	$\beta$ : 1.29/1,000
SI: 285	MI: 250

- 2.) Solve:

VOLT_TL.VU	0.700000000016 $\angle$ -6.77682980664
VOLT_TL.VL	0.419999999984 $\angle$ -11.3423365418
VOLT_TL.TVSI	0.599999999963

- Answer:  
 $\phi_u = -6.8$  degrees

- 3.) Triangle visualisation:



# Normal Voltages, Leading PF Load with TVSI=0.6

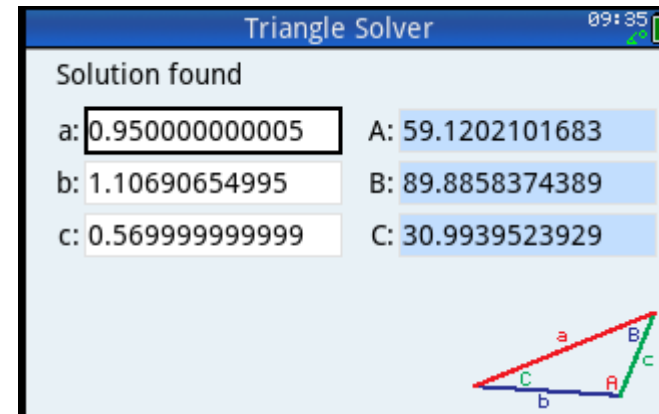
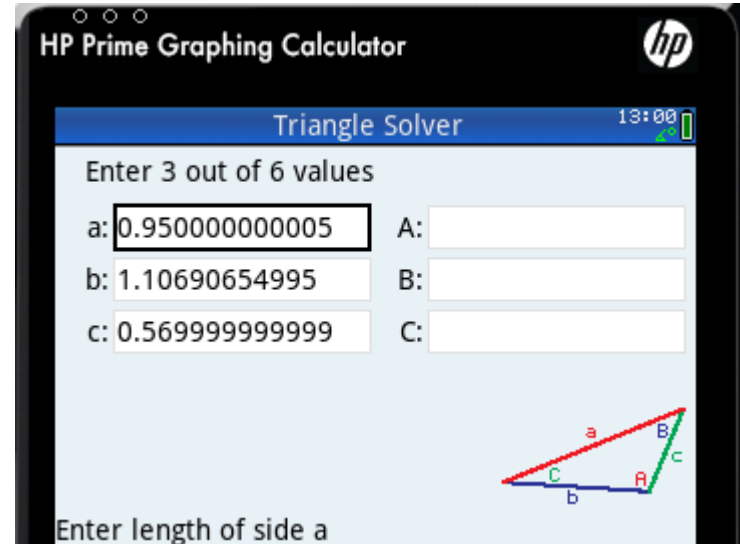
- 1.) Given:

E: 1.05	KV: 345
P: 6.7484687254	Q: -0.3839815...
$\alpha$ : 0.066/1,000	$\beta$ : 1.29/1,000
SI: 285	MI: 250

- 2.) Solve:

VOLT_TL.VU	0.950000000006 $\angle$ -30.9939523928
VOLT_TL.VL	0.569999999999 $\angle$ -59.1202101682
VOLT_TL.TVSI	0.599999999995

- 3.) Triangle visualisation:



- Answer:  
 $\phi_u = -31$  degrees



# Normal Voltages, Leading PF Load with TVSI=0.6

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- Bus voltages can look good and yet TVSI can be relatively high!
- **Phase angles** can provide an indication of the TVSI level for **Normal Voltages**.

# Phase Angles as a Proxy for Voltage Stability

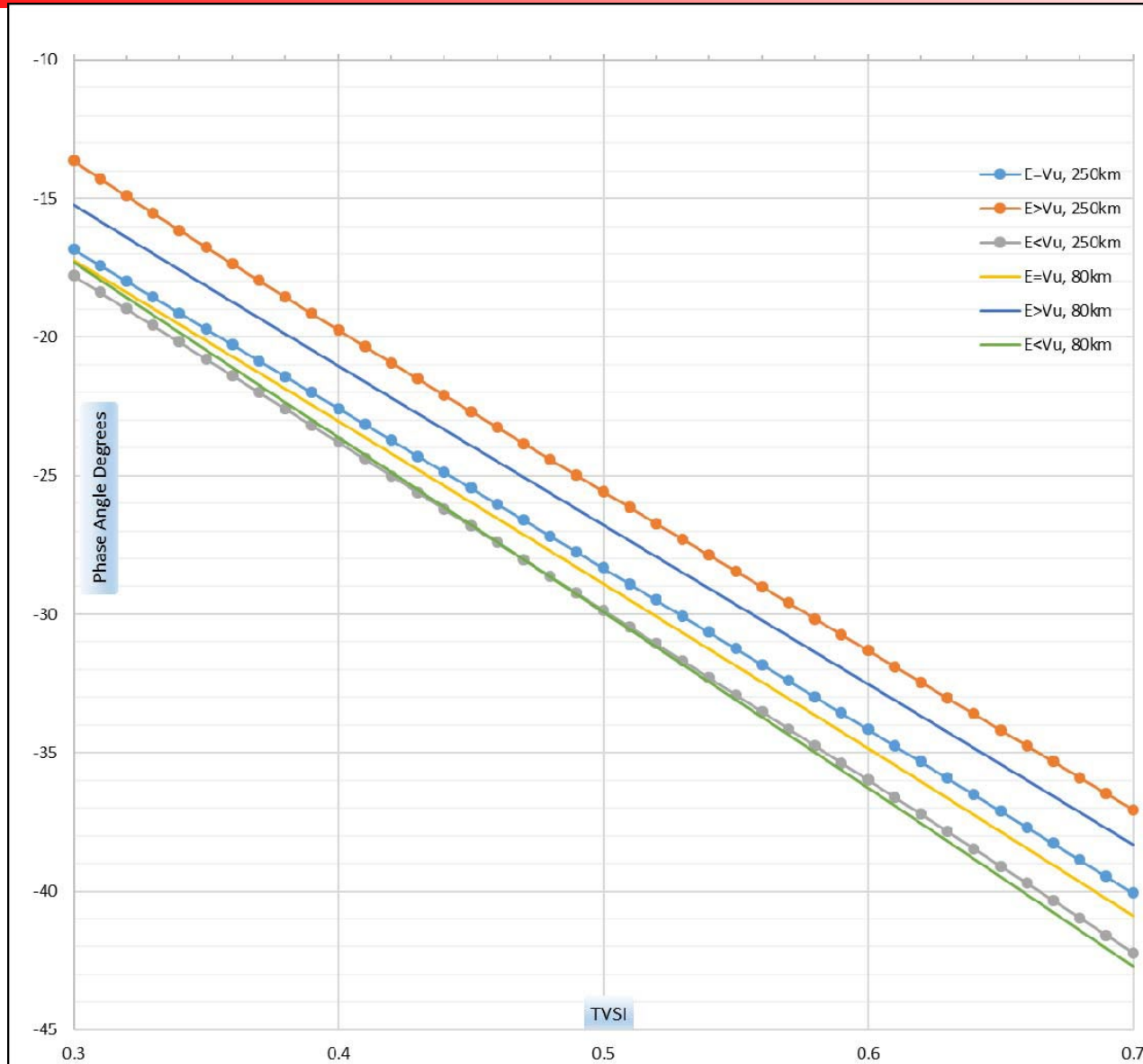
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- Existing real time State Estimator tools in the AEP control room already address low voltage magnitudes and voltage drop limitations outside the normal voltage range.
- We establish the **phase angle loci** associated with a Triangle Voltage Stability Index (TVSI) for EHV voltages in the normal range of 0.95 - 1.05PU range.
- Compare the established **phase angle** against a PSSE TVSI study.

# Phase Angles as a Proxy for Voltage Stability

- On next two sides...
  - Display **Phase Angles** vs TVSI
    - $0.95 \text{ PU} < E < 1.05 \text{ PU}$
    - $0.95 \text{ PU} < V_u < 1.05 \text{ PU}$ 
      - For  $E=1.05$  and  $V_u=0.95$  there would be about a 10% voltage deviation.
  - Compare established **phase angle loci** against a PSSE TVSI study.

# Phase Angles vs TVSI



# Comparison of PSSE Phase Angles to Phase Angle Loci

PSSE TVSI Study							Phase Angle Loci for given PSSE TVSI
From bus	To bus	TVSI	BASE kV	Difference Angle in Degrees	Contingency	Case	Angle Range Degrees <sup>2</sup>
A	C	0.6784	138	-38.9°	N -V 345kV + L -V 345kV	2018 Summer SPA South -North transfer	-35.8°, -40.6°
N	V	0.45817	345	-26.3°	L -V 345kV + M -F 345kV	2018 Summer SPA South -North transfer	-23.2°, -27.3°
P	V	0.41695	345	-23.6°	H -S 345kV + E	2018 Summer SPA South -North transfer	-20.7°, -24.7°
N	W	0.34818	345	-19.2°	L -W 345kV + R -C 345kV	2018 Summer SPA South -North transfer	-16.6°, -20.3°
D	S	0.65237	345	-37.9°	J -R 765kV + D -E 345kV	2018 Summer SPA West -East transfer	-34.3°, -39.6°
D	S	0.53417	345	-30.7°	J -R 765kV	2018 Summer SPA West -East transfer	-27.5°, -32.1°
K	M	0.4547	345	-26.4°	C -J 765kV	2018 Winter SPA North -Southeast transfer	-23.°, -27.1°
K <sup>1</sup>	M	0.3805	345	-21.9°	C -J 765kV	2018 Winter SPA North - Southeast transfer	-18.6°, -22.4°

# Conclusions

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- AEP uses **phase angles** as a proxy for voltage stability using EHV voltages in the normal range of 0.95 to 1.05 PU to provide situational awareness to system operators on key circuits.
- Existing real time tools in the AEP control room already address low voltage magnitudes and voltage drop limitations outside the normal voltage range.

# Appendix - Voltage Stability Triangle Program

```

1 //HP PRIME CALCULATOR
2 // Transmission Long Line Load Flow
3 // W.D. Stevenson, Jr Elements of Power System Analysis, 4th ed.
4 // (New York: McGraw-Hill, 1982)
5 // Based on  $V_S = V + \text{Cosh}((\alpha + j\beta)mi) + ZcI + \text{Sinh}((\alpha + j\beta)mi)$  equation in
6 // Stevenson's book.
7 // E - PU sending voltage
8 // KV - Base KV
9 // P+jQ - PU receiving load
10 //  $\alpha + j\beta$  - Propagation Constant / MI
11 // SI - Surge Impedance in Ohms
12 //Michael R Richardson 8/2/2018
13 //
14 EXPORT ET,VU,VL,p,VUn,VLn,Vs,Is;
15 EXPORT TVSI;
16 EXPORT VOLT_TL(E,KV,P,Q, $\alpha$ , $\beta$ ,SI,MI)
17 BEGIN
18 LOCAL VR,VI,VRL,Z,W,Ir;
19 HComplex:=1;
20 HAngle:=1;
21 W:= $\text{COSH}((\alpha,\beta)*MI)$ ;
22 Z:= $SI + \text{SINH}((\alpha,\beta)*MI) / ((KV^2/100.))$ ;
23
24 p:=( $\text{CONJ}((P,Q))*Z/W$ );
25 ET:= $E/ABS(W)$ ;
26 SideB:=ET;
27 VI:=- $IM(p)/ABS(ET)$ ;
28  $\Delta := ABS(ET/2.)^2 - RE(p) - (VI^2)$ ;
29 IF  $\Delta < 0$ . THEN
30   HAngle:=0;
31   RETURN "No solution  $\Delta =$ " +  $\Delta$ ;
32 END;
33 Z5:=(P,Q);
34
35  $\Delta := \sqrt{\Delta}$ ;
36 VR:= $ABS(ET)/2. + \Delta$ ;
37 VRL:= $ABS(ET)/2. - \Delta$ ;
38 VU:=(VR,VI);
39 VL:=(VRL,VI);
40 VUn:=(VR,VI)/ $normalize(W)$ ;
41 VLn:=(VRL,VI)/ $normalize(W)$ ;
42 SideA:= $ABS(VUn)$ ;
43 SideC:= $ABS(VLn)$ ;
44 Ir:=  $\text{CONJ}( (P,Q) ) / \text{CONJ}(VUn)$ ;
45 Vs:= $VUn*W + Ir*Z$ ;
46 Is:= $Ir*W + VUn*\text{SINH}((\alpha,\beta)*MI)*KV^2/(SI*100)$ ;
47 //TVSI:= $ABS(VL/VU)$ ;
48 Z6:=  $Vs/Is$ ; //Z @ SOURCE END
49 Z1:= $W*VUn + Z*(P,-Q)/\text{CONJ}(VUn)$ ;
50 Z2:= $W*VLn + Z*(P,-Q)/\text{CONJ}(VLn)$ ;
51 Z7:= $SI + \text{SINH}((\alpha,\beta)*MI)$ ;
52 Z9:=  $W$ ; // $\text{COSH}()$ 
53 TVSI:=  $ABS(VL/VU)$ ;
54 Z8:=  $2*ABS(W)^2 * ABS(p) * (1 + \text{COS}(ARG(p)))$ ;
55 Z8:=  $\sqrt{Z8}$ ; //Ec -critical sending in voltage
56 HAngle:=0;
57 RETURN  $ABS(VUn) + " \angle " + ARG(VUn) + " \Delta =$ " +  $\Delta$ ;
58
59 END;
60

```