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# PESCRIPTIONS FOR THE POWER GRID IN THE DIGITAL AGE

# WideBand Voltage Sensors For The Modern Substation

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#### Presentation Outline

- Introduction
- Impacts To The High Voltage Equipment In A Network
- Types Of Instrument Transformers For Voltage Measurement
- Theoretical Aspects of RC-Dividers
- Frequency Response Behavior Of RC-Dividers
- Conclusions



#### Introduction

#### Generation





#### Harmonic Emissions – Per IEEE 519 Limits





#### Other Emission Sources

Equipment	Voltage dips	Voltage swells	Harmonics	Interharmonics	Subharmonics	Supraharmonics	Slow voltage variations	Fast voltage variations	Transients	Voltage unbalance	Frequency variations	DC components
PV inverters	X											
Production units	X										X	
Active converters	X	x	x	x	x	X	X	X	X	X	X	X
LED lamps				x				X				
Power line communication						X			X			
Transformers						X			X			
Rotating machines						X			X			
Cable insulation						X						
Instrument transformers						X						
Three-phase converters										X		



#### Frequency Content





### Impacts To The High Voltage Equipment In A Network

- Increasing of power losses within the network
- Increasing electric stresses within the HV insulation system (permanently as well as transient)
- Thermal stresses within the connected equipment due to harmonic currents
- Increasing sound noise emission (transformers, coils, capacitors, etc.)
- Incorrect control of equipment

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- Faulty activation of protection equipment (old protection system)
- Forced aging of high voltage equipment

### Types Of Instrument Transformers For Voltage Measurement

- Potential Transformer (PT)
  - Magnetically Coupled
  - Most Frequently Used
- Capacitive Coupled Voltage Transformer (CCVT)
  - As the name suggests capacitive coupling
  - Mature technology, but less frequently used
- Optically Coupled Voltage Transformer
  - Uses Faraday effect.
  - In Development.

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#### Frequency Response – Magnitude Accuracy



Legend 36kV-VT(light green) 72.5kV-VT(dark green) 123kV-VT(blue) 245kV-VT(purple) 420kV-CTVT(red) 420kV-RC-divider (yellow)



#### Frequency Response – Phase Shift Error



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Legend 36kV-VT(light green) 72.5kV-VT(dark green) 123kV-VT(blue) 245kV-VT(purple) 420kV-CTVT(red) 420kV-RC-divider (yellow)



V<sub>1</sub>: Primary voltage
V<sub>2</sub>: Secondary voltage
C<sub>1</sub>: Primary capacitance
R<sub>1</sub>: Primary resistance
C<sub>2</sub>: Secondary capacitance
R<sub>2</sub>: Secondary resistance
i<sub>C</sub>: Capacitive current
i<sub>R</sub>: Resistive current



$$\underline{Z}_{1} = \frac{R_{1}}{1 + j\omega C_{1}R_{1}}$$
$$\underline{Z}_{2} = \frac{R_{2}}{1 + j\omega C_{2}R_{2}}$$
$$\underline{Z}_{1} = \frac{R_{1}}{1 + j\omega C_{1}R_{1}} + \frac{R_{2}}{1 + j\omega C_{2}R_{2}}$$





$$\underline{k}_{C}(j\omega) = \frac{C_{1}}{C_{1} + C_{2} \cdot \frac{(1 + 1/(j\omega C_{2}R_{2}))}{(1 + 1/(j\omega C_{1}R_{1}))}}$$

$$\underline{k}_{R}(j\omega) = \frac{R_{2}}{R_{2} + R_{1} \cdot \frac{(1 + j\omega C_{2}R_{2})}{(1 + j\omega C_{1}R_{1})}}$$

$$\begin{pmatrix} f \to \infty \\ \frac{Z_{2}}{Z_{\text{total}}} = \frac{C_{1}}{C_{1} + C_{2}} \end{pmatrix}$$

$$\begin{pmatrix} f \to 0 \\ \frac{Z_{2}}{Z_{\text{total}}} = \frac{R_{2}}{R_{2} + R_{1}} \end{pmatrix}$$





$$\tau_1 = \tau_2 \rightarrow R_1 \cdot C_1 = R_2 \cdot C_2$$

1.  $\tau_1 > \tau_2$ , undercompensated 2.  $\tau_1 = \tau_2$ , compensated 3.  $\tau_1 < \tau_2$ , overcompensated

In case 2, the secondary voltage follows the primary voltage with a fixed time delay:

$$T_{\rm a}=2.2\cdot\tau_1=2.2\cdot\tau_2$$



 For a variety of reasons, it is not possible to perfectly match the primary and secondary components, therefore:

• 
$$\tau_1 \neq \tau_2 \rightarrow R_1 \cdot C_1 \neq R_2 \cdot C_2$$

• Frequency-dependent error formulas may be derived.





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Legend Type: AIS RC-divider Voltage accuracy – blue Phase displacement – green



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Legend Type: GIS RC-divider Voltage accuracy – blue Phase displacement – green



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**Legend** Type: GIS RC-divider Input Signal: Impulse Reference – Blue Measured – Red



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Legend Type: AIS RC-divider Input Signal: Step Response Reference – Blue Measured – Red

#### Conclusions

- The grid is becoming a "more noisy" place.
- Traditional measurement transformers may lack the bandwidth to accurately observe phenomenon on the grid.
- There are new types of measurement transformers which provide adequate frequency response with low measurement error.
- Final thought present standards may not have accuracy classes which cover all of the necessary functions in the modern grid: revenue metering, protection, power quality measurement, etc.



# Questions?





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