



STATE ESTIMATION IN DISTRIBUTION SYSTEMS

2015 CIGRE Grid of the Future Symposium
Chicago (IL), October 13, 2015

L. Garcia-Garcia, D. Apostolopoulou

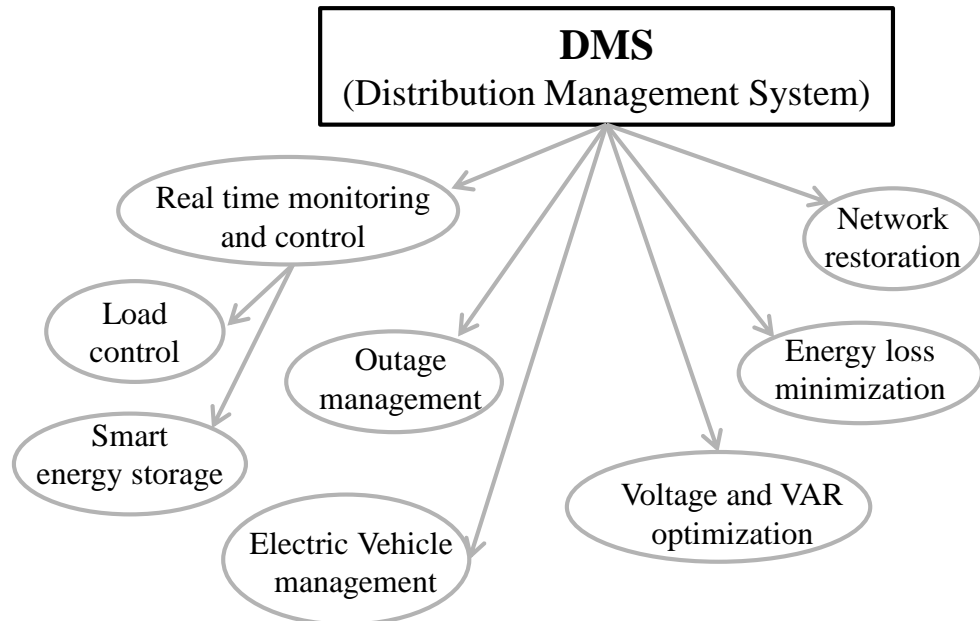
Laura.GarciaGarcia@ComEd.com

Dimitra.Apostolopoulou@ComEd.com

What has been done...

We developed and tested a State Estimation approach for Distribution Systems, as well as a sensitivity analysis to test the robustness of the method

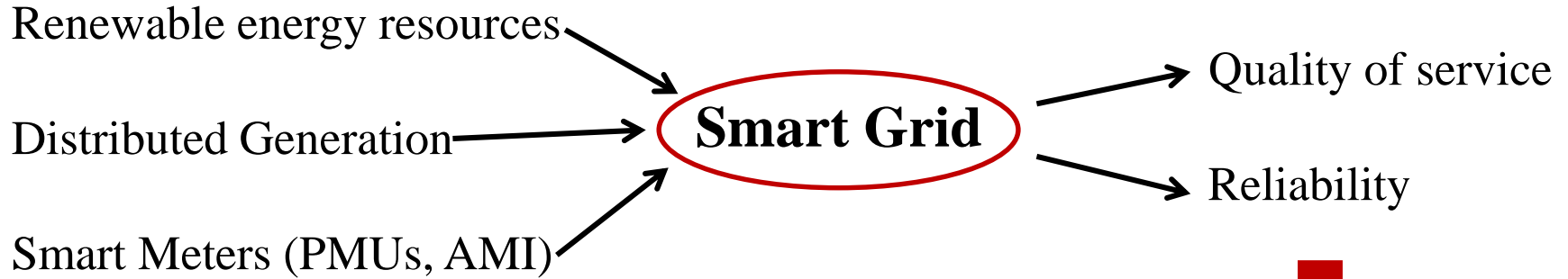
...has multiple applications



Outline

- Smart Distribution Systems
- Challenges in Distribution Systems
- State Estimation Overview
- Use of WLS for State Estimation
- WLS State Estimation in Distribution Systems
- Case Study – IEEE 34-Bus Test System
 - Numerical results
 - Sensitivity analysis
 - Sensitivity analysis results
- Conclusions

Smart Distribution Systems



State Estimation (SE):

Provides State of the Grid in real-time for **monitoring** and **control**:

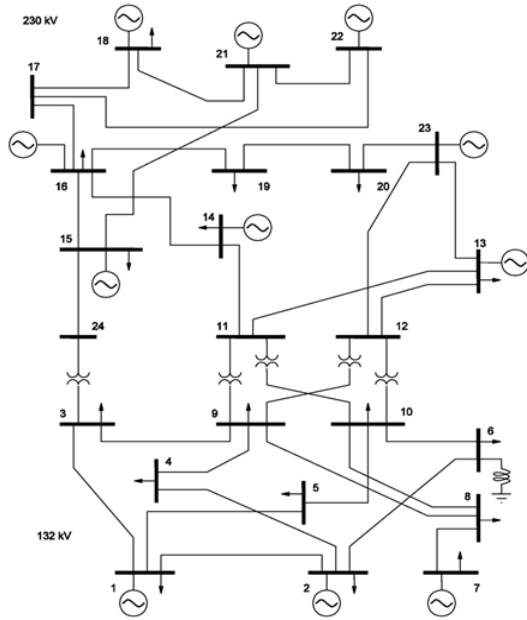
- Online contingency analysis
- Bad data detection
- Power Flow Optimization

Challenges in Distribution Systems

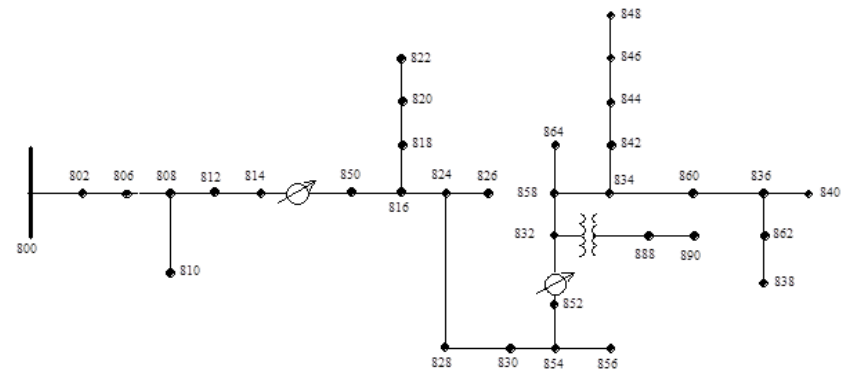
Transmission System

vs

Distribution System



IEEE 24 Bus Test System



IEEE 34 Bus Test System

Meshed topology

Uni-directional power flows

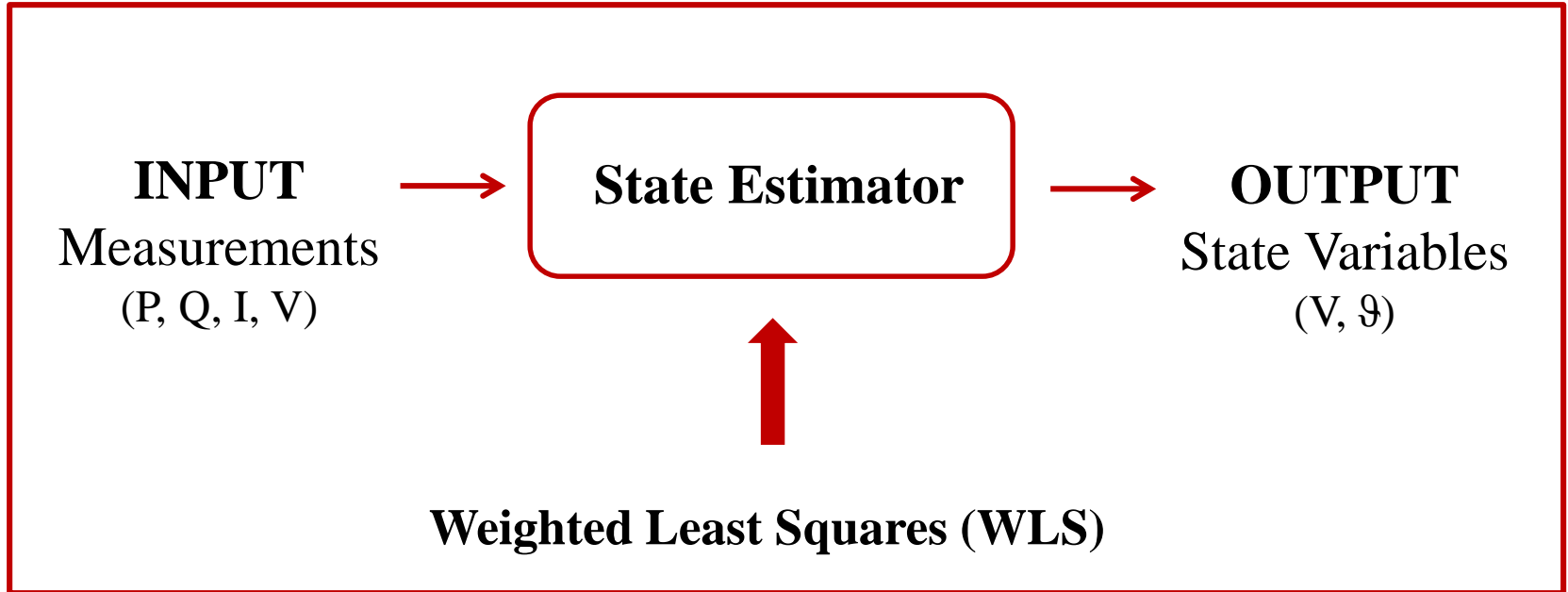
Balanced lines and loads

Radial topology

Bi-directional power flows

Unbalanced lines and loads

State Estimation Overview



Advantages

- Overdetermined System
- Performs well in presence of noise

Disadvantages

- Fails to reject bad data
- Sensitive to initial point



Observability → pseudo-measurements

Use of WLS for State Estimation (1/2)

✓ Weighted Least Squares:

$$z = h(x) + e$$

z : measurement vector e : measurement errors (Gaussian distribution)
 x : state variables vector $h(x)$: measurement function

$$r = z - h(x)$$

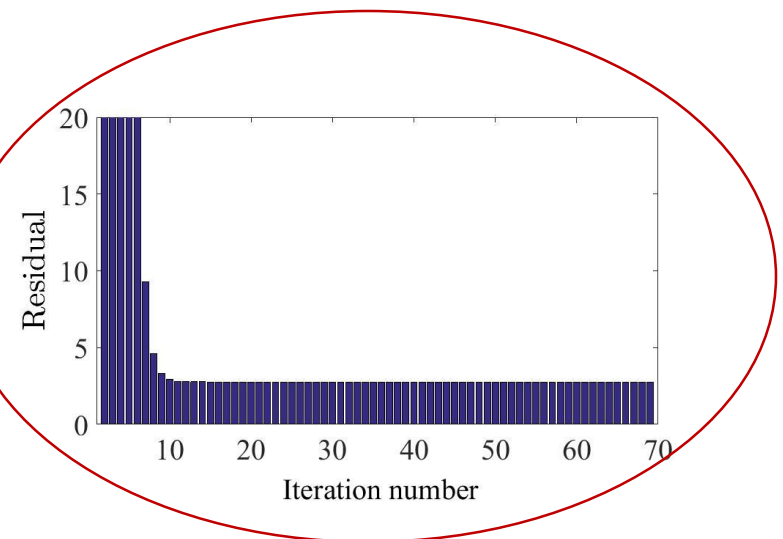
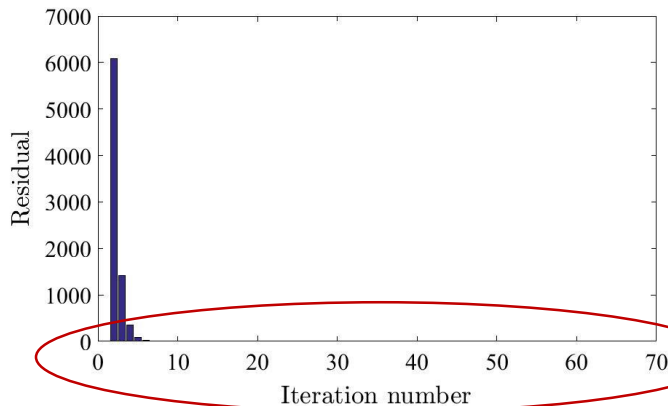
r : residual error W : penalty factor of measurements

Optimization problem:

$$\min_x J(x) = [z - h(x)]^T W [z - h(x)]$$



$$\begin{aligned} H^T(x)W[z - h(x)] &= 0 \\ H(x) &= \frac{\partial h(x)}{\partial x} \end{aligned}$$



Use of WLS for State Estimation (2/2)

✓ Iterative Process:

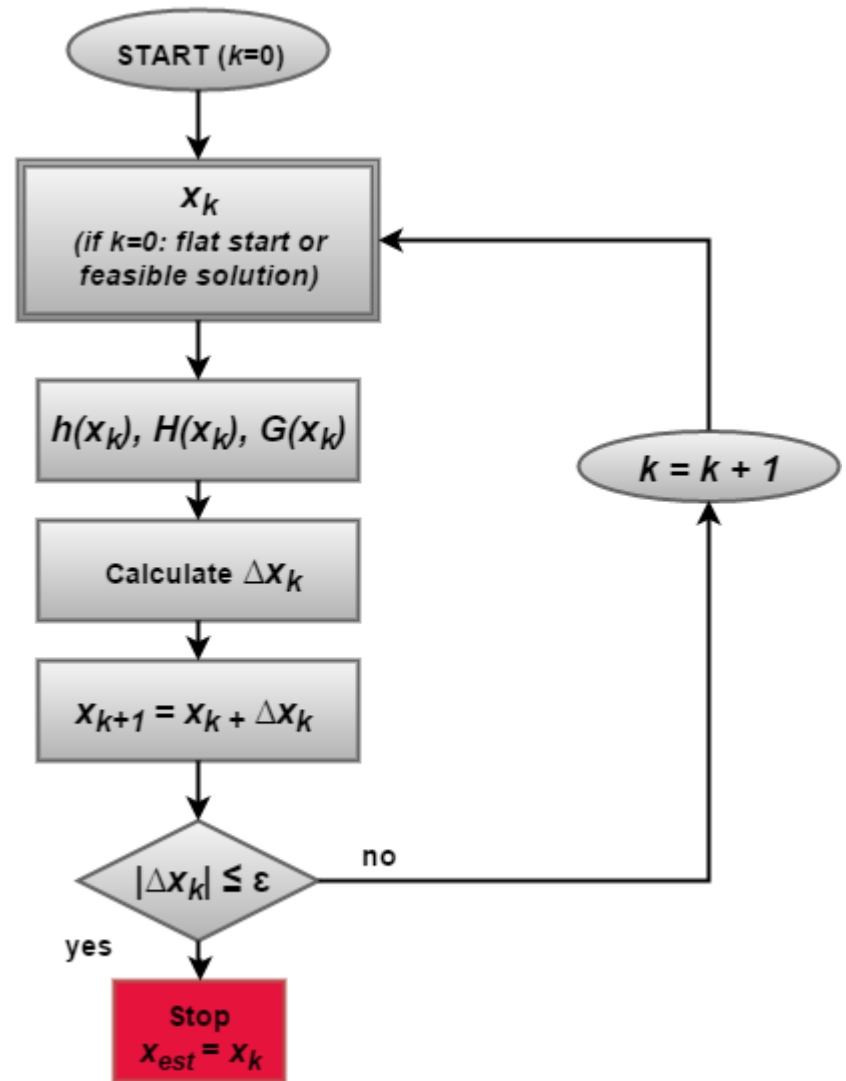
$$x_{k+1} = x_k + \Delta x_k$$

given that the increment Δx_k is given by

$$[G(x_k)]\Delta x_k = H^T(x_k)W[z - h(x_k)]$$

where

$$G(x) = H^T(x)WH(x)$$



WLS State Estimation in Distribution Systems

Measurements and
State Variables vectors

$$z = [P^f{}^T, Q^f{}^T, I_l{}^T, V_m{}^T, P^T, Q^T, P_L{}^T, Q_L{}^T]^T \quad x = [V_m{}^T, \theta^T]^T$$

Jacobian Matrix of
the State Equations

$$H(x) = \begin{bmatrix} \frac{\partial P^T}{\partial V} & \frac{\partial Q^T}{\partial V} & \frac{\partial I_l{}^T}{\partial V} & \frac{\partial V_m{}^T}{\partial V} & \frac{\partial P^T}{\partial V} & \frac{\partial Q^T}{\partial V} & \frac{\partial P_L{}^T}{\partial V} & \frac{\partial Q_L{}^T}{\partial V} \\ \frac{\partial P^T}{\partial \theta} & \frac{\partial Q^T}{\partial \theta} & \frac{\partial I_l{}^T}{\partial \theta} & \frac{\partial V_m{}^T}{\partial \theta} & \frac{\partial P^T}{\partial \theta} & \frac{\partial Q^T}{\partial \theta} & \frac{\partial P_L{}^T}{\partial \theta} & \frac{\partial Q_L{}^T}{\partial \theta} \end{bmatrix}^T$$

Penalty factors matrix

$$W_{ii} = \begin{cases} 1 & \text{For the forecasted load} \\ 10 & \text{For the actual measurements} \end{cases}$$

P^f Forecasted real injection

Q^f Forecasted reactive injection

I_l Line current measurements

V_m Voltage magnitudes

θ_m Voltage angles

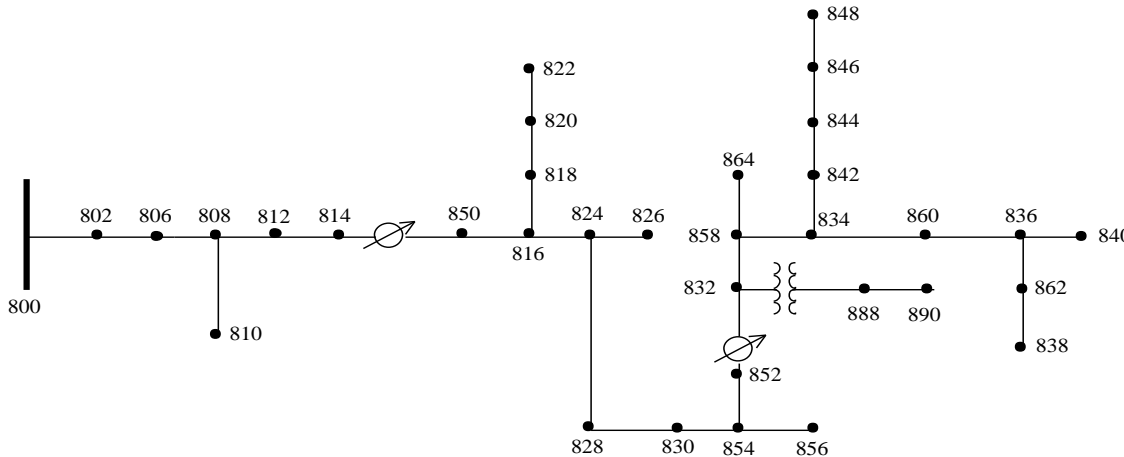
P_L : Real bus withdrawals at load nodes

Q_L : Reactive bus withdrawals at load nodes

P : Real bus injections at generator nodes

Q : Reactive bus injections

Case Study – IEEE 34-Bus Test System



24.9 kV
Radial feeder
Some single-phase laterals
but mostly 3-phase

Scenario 1 set of measurements:

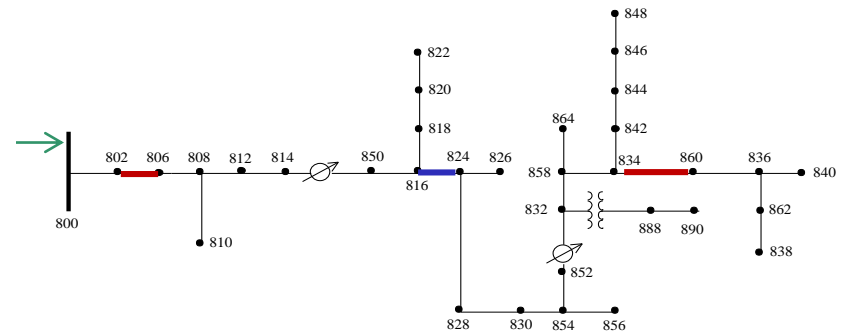
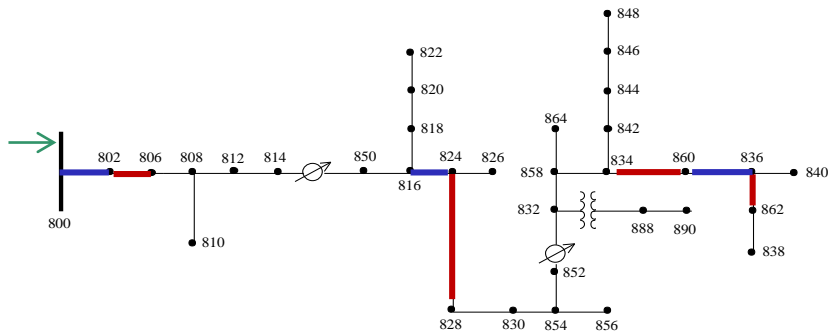
- Forecasted load with 10% of perturbation
- Power injection measurement at substation
- Power flow of lines 802-806, 824-828, 834-860, 836-862
- Line current of lines 800-802, 816-824, 860-836

Scenario 2 set of measurements:

- Forecasted load with 10% of perturbation
- Power injection measurement at substation
- Power flow measurements of lines 802-806, 834-860
- Line current measurements of line 816-824

→ We test the performance of the State Estimator in two different scenarios, including different quantity of measurements each time.

Case Study – Numerical results



Scenario 1

- Algorithm converged in **69** iterations
- Residual for the last iteration:
$$r = z - h(x) = \mathbf{2.7494}$$
- Maximum difference between estimated and actual voltage magnitude value is **0.09 pu**

Scenario 2

- Algorithm converged in **67** iterations
- Residual for the last iteration:
$$r = z - h(x) = \mathbf{2.5293}$$
- Maximum difference between estimated and actual voltage magnitude value is **0.095 pu**

✓ Results are very similar in both cases.

✓ The method results in a **feasible solution** for the estimate of the state variables

Case Study – Sensitivity analysis

Motivation: Test the robustness of the algorithm and sensitivity to bad quality input data.

Relative error of
voltage magnitudes
at each bus

$$\text{Error} = \frac{V_{estimate} - V_{actual}}{V_{actual}} \times 100\%$$

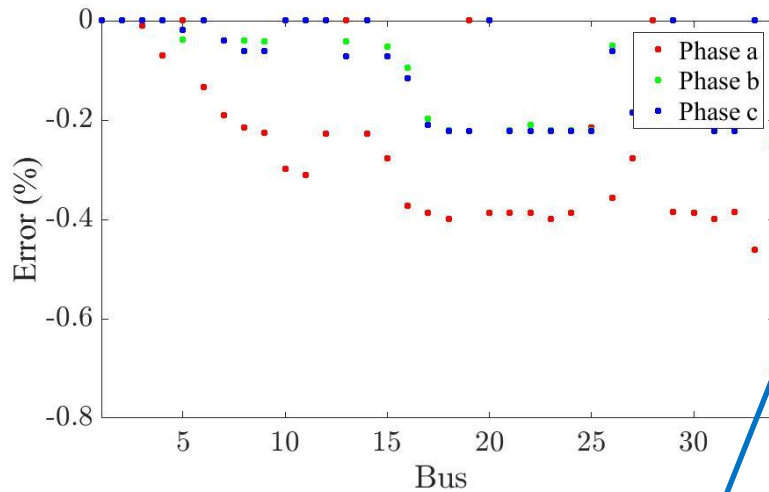
Simulation of bad quality data recreated in 4 different cases:

- **Case 1:** Increased the line power flow measurements by 2.5%
- **Case 2:** Increased the line power flow measurements by 10%
- **Case 3:** Increased the power flow and line current measurements by 2.5%
- **Case 4:** Increased the power flow and line current measurements by 10%

Case Study – Sensitivity analysis results (1/4)

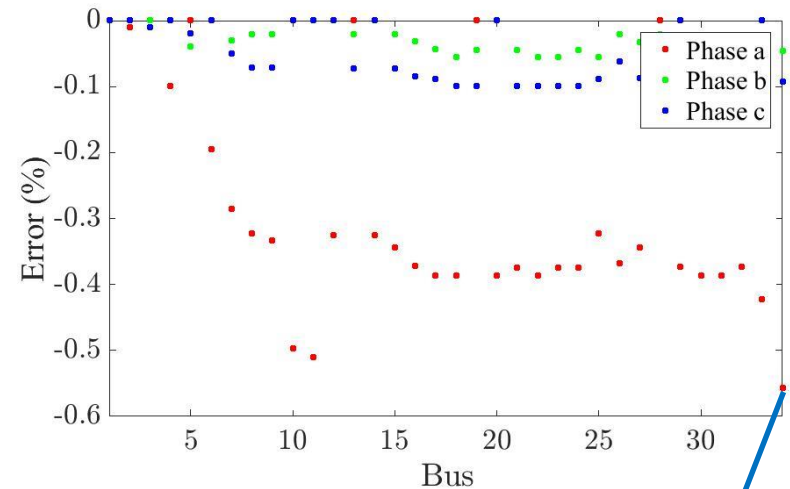
Case 1: Increased the line power flow measurements by 2.5%

➤ Voltage magnitude error for Scenario 1



Max. Error = -0.71%

➤ Voltage magnitude error for Scenario 2

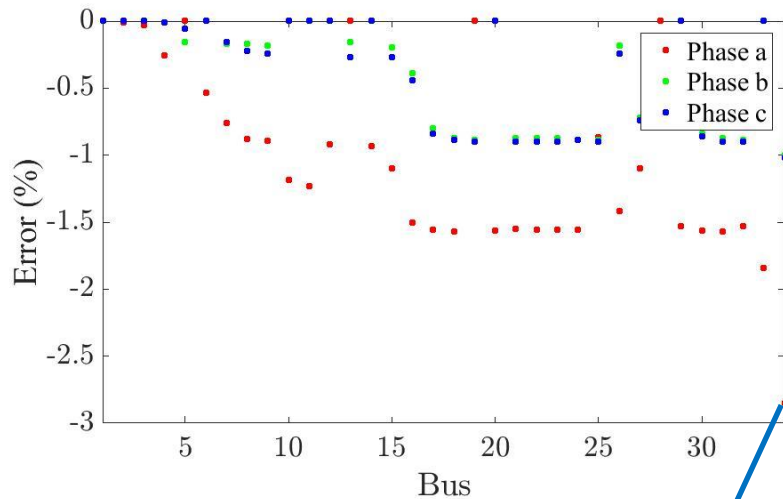


Max. Error = -0.56%

Case Study – Sensitivity analysis results (2/4)

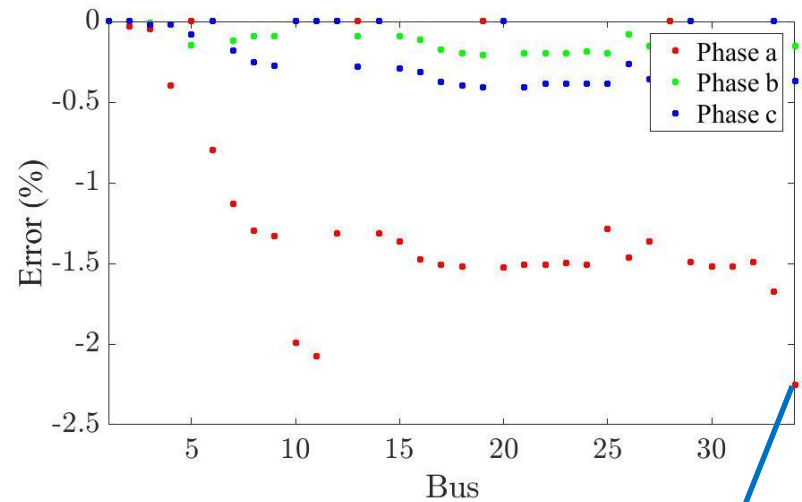
Case 2: Increased the line power flow measurements by 10%

➤ Voltage magnitude error for Scenario 1



Max. Error = -2.85%

➤ Voltage magnitude error for Scenario 2

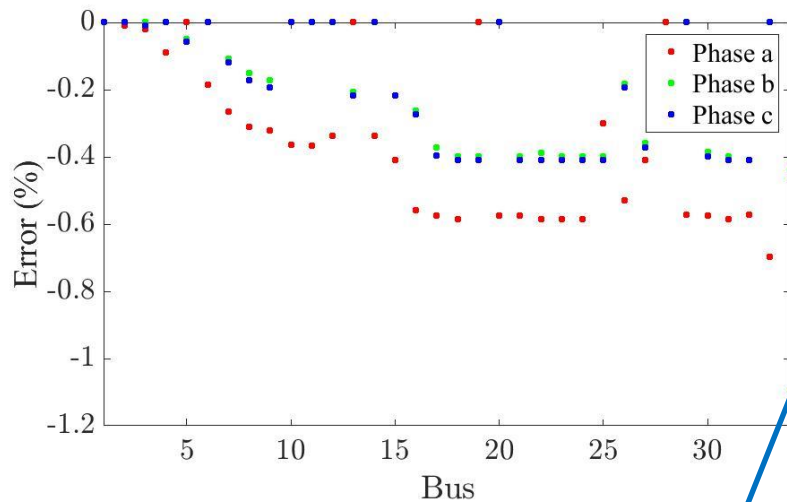


Max. Error = -2.26%

Case Study – Sensitivity analysis results (3/4)

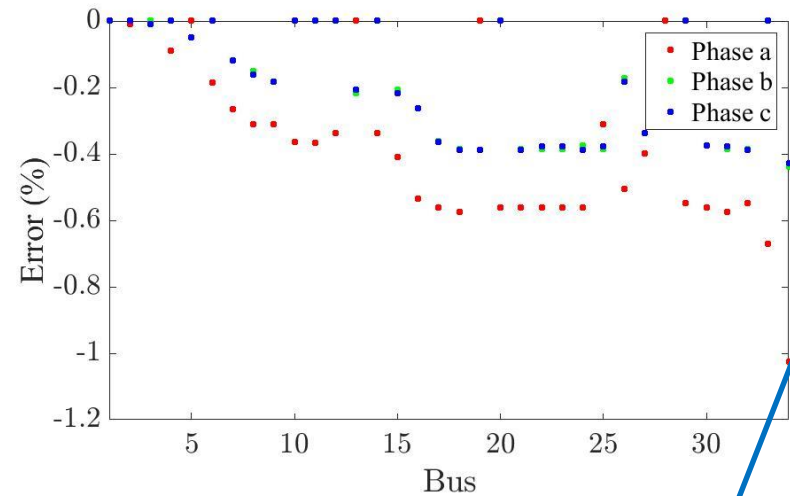
Case 3: Increased the line power flow and line current measurements by 2.5%

➤ Voltage magnitude error for Scenario 1



Max. Error = -1.09%

➤ Voltage magnitude error for Scenario 2

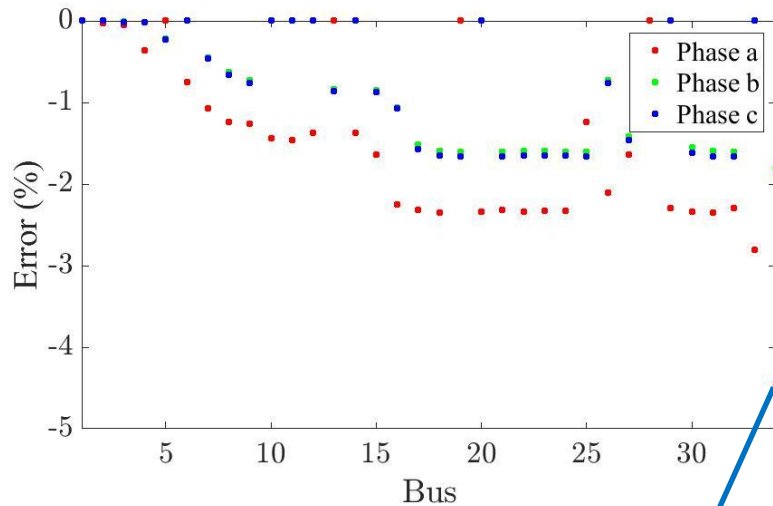


Max. Error = -1.03%

Case Study – Sensitivity analysis results (4/4)

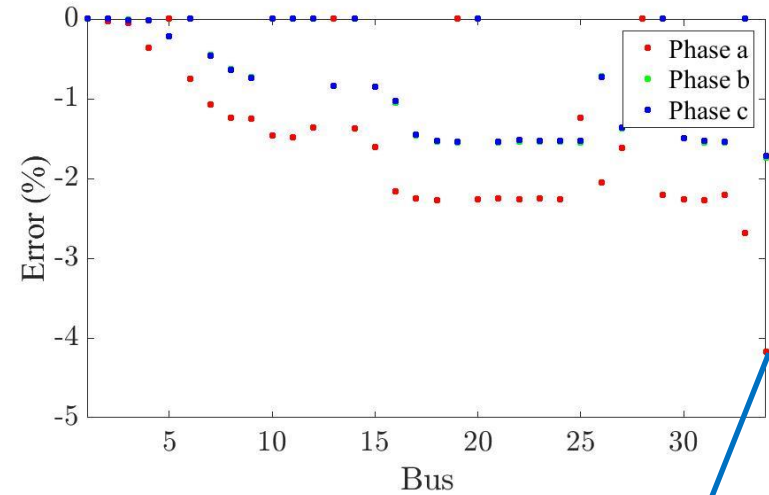
Case 4: Increased the line power flow and line current measurements by 10%

➤ Voltage magnitude error for Scenario 1



Max. Error = -4.46%

➤ Voltage magnitude error for Scenario 2



Max. Error = -4.17%

Summary of Sensitivity analysis results

- Absolute error in the results:

Error Introduced	Scenario	+2.5%	+10%
Power Flow Measurements	1	0.71%	2.85%
	2	0.56%	2.26%
Power Flow and Current Measurements	1	1.09%	4.46%
	2	1.03%	4.17%

Conclusions

- SE is a powerful tool that has been traditionally used in Transmission Systems. Its application for Distribution Systems is feasible today and would enhance grid operation and planning.
- The traditional approach to this method, the WLS algorithm, can be implemented to Distribution Systems taking into account the specific characteristics of these systems.
- The tool created based on WLS algorithm showed encouraging results when applied to different Scenarios of the IEEE 34 Bus Test System.
- This algorithm is robust and still present good results under the “bad quality data” simulation.
- Application to a real feeder is currently under study, as well as other possible approaches to the State Estimation problem.

Thank you!